

Higher-order sliding-mode observer for state estimation and input reconstruction in nonlinear systems

Leonid Fridman¹, Yuri Shtessel^{2,*†}, Christopher Edwards³ and Xing-Gang Yan³

¹ *Division de Ingenieria Electronica, Facultad de Ingenieria, National Autonomous University of Mexico, UNAM, 04510, Mexico, D.F., Mexico*

² *Department of Electrical and Computer Engineering, The University of Alabama in Huntsville, Huntsville, AL 35899, U.S.A.*

³ *Control & Instrumentation Group, Department of Engineering, University of Leicester, Leicester LE17RH, U.K.*

SUMMARY

Step-by-step vector-state reconstruction by means of sliding modes has been presented in [2, 7–9]. These observers are based on a transformation to a triangular or the Brunovsky canonical form and successive estimation of the state vector using the equivalent output error injection. The corresponding conditions for linear time-invariant systems with unknown inputs were obtained in [4, 9–11]. Moreover, the above-mentioned observers theoretically ensure finite-time convergence for all system states. Unfortunately, the realization of step-by-step observers is based on conventional sliding modes, leading to filtration at each step due to discretization or non-idealities of the analog devices used to implement the schemes. In order to avoid the necessity for filtration, hierarchical observers were recently developed in [10, 12] iteratively using the continuous super-twisting algorithm, based on second-order sliding-mode ideas [13].

The super-twisting structure is also used in the modified version of the step-by-step observer in [9]. Unfortunately, these observers are also not free of drawbacks: the super-twisting algorithm provides the best possible asymptotic accuracy of the derivative estimation at each single realization step [13]. In particular, the accuracy is proportional to the sampling step δ for the discrete realization in the absence of noise, and to the square root of the input noise magnitude if the discretization error is negligible. The step-by-step and hierarchical observers use the output of the super-twisting algorithm as a noisy input at the next step. As a result, the overall observation accuracy is of the order δ

Assumptions (Isidori [15])

At a neighbourhood of any point $x \in \Omega$

- (i) The system in (1) is assumed to have a vector relative degree $r = \{r_1, r_2, \dots, r_m\}$, i.e.

$$\begin{aligned} L_{g_j} L_f^k h_i(x) &= 0 \quad \forall j = 1, \dots, m \quad \forall k < r_i - 1 \quad \forall i = 1, \dots, m \\ L_{g_j} L_f^{r_i-1} h_i(x) &\neq 0 \quad \text{for at least one } 1 \leq j \leq m \end{aligned} \quad (2)$$

- (ii) The $m \times m$ matrix

$$E(x) = \begin{bmatrix} L_{g_1}(L_f^{r_1-1} h_1) & L_{g_2}(L_f^{r_1-1} h_$$

3.1. Coordinate transformation

The system given by (1)–(3) with an involutive distribution $\Gamma = \text{span}\{g_1, g_2, \dots, g_m\}$ and total relative degree $r = \sum_{i=1}^m r_i < n$ can be presented in a new basis that is introduced as follows:

$$\{\xi^T, \eta^T\}^T : \xi^i = \begin{pmatrix} \xi_1^i \\ \xi_2^i \\ \vdots \\ \xi_{r_i}^i \end{pmatrix} = \begin{pmatrix} \phi_1^i(x) \\ \phi_2^i(x) \\ \vdots \\ \phi_{r_i}^i(x) \end{pmatrix} = \begin{pmatrix} h_i(x) \\ L_f h_i(x) \\ \vdots \\ L_f^{r_i-1} h_i(x) \end{pmatrix} \in \mathfrak{R}^{r_i} \quad \forall i = 1, \dots, m$$

$$\xi = \begin{pmatrix} \xi^1 \\ \xi^2 \\ \vdots \\ \xi^m \end{pmatrix}, \quad \eta = \begin{pmatrix} \eta_1 \\ \eta_2 \\ \vdots \\ \eta_{n-r} \end{pmatrix} = \begin{pmatrix} \phi_{r+1}(x) \\ \phi_{r+2}(x) \\$$

where

$$\Lambda_i = \begin{bmatrix} 0 & 1 & 0 & \dots & 0 \\ 0 & 0 & 1 & \dots & 0 \\ \vdots & \vdots & \vdots & \dots & \vdots \\ 0 & 0 & 0 & 0 & 0 \end{bmatrix} \in \mathfrak{R}^{r_i \times r_i}, \quad \psi^i(\zeta, \eta) = \begin{pmatrix} 0 \\ 0 \\ \vdots \\ L_f^{r_i} h_i(x) \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ \vdots \\ L_f^{r_i} h_i(\Phi^{-1}(\zeta, \eta)) \end{pmatrix}$$

$$\lambda^i(\zeta, \eta, \varphi(t)) = \begin{pmatrix} 0 \\ 0 \\ \vdots \\ \sum_{j=1}^m L_{g_j} L_f^{r_i-1} h_i(x) \varphi_j(t) \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ \vdots \\ \sum_{j=1}^m L_{g_j} L_f^{r_i-1} h_i(\Phi^{-1}(\zeta, \eta)) \varphi_j(t) \end{pmatrix} \quad \forall i = 1, \dots, m$$

- the distribution $\Gamma = \text{span}\{g_1, g_2, \dots, g_m\}$ is involutive;
- the internal dynamics (12) are locally asymptotically stable.

The derivatives $\xi_j^i(t) \forall i = 1, \dots, m \forall j = 1, \dots, r_i$ of the measured outputs $y_i = h_i(x)$ can be estimated in finite time by the higher-order sliding-mode differentiator [14]. This can be written in the form

$$\begin{aligned}
 \dot{z}_0^i &= v_0^i \\
 v_0^i &= -\lambda_0^i |z_0^i - y_i(t)|^{(r_i/(r_i+1))} \text{sign}(z_0^i - y_i(t)) + z_1^i \\
 \dot{z}_1^i &= v_1^i \\
 v_1^i &= -\lambda_1^i |z_1^i - v_0^i|^{((r_i-1)/r_i)} \text{sign}(z_1^i - v_0^i) + z_2^i \\
 &\vdots \\
 \dot{z}_{r_i-1}^i &= v_{r$$

(unobservable) solution $\eta(t)$ that passes through an unknown initial condition $\eta(t_0)$. In other words, the asymptotic estimate $\hat{\eta}(t)$ of $\eta(t)$ can be obtained locally:

$$\hat{\eta} = \begin{pmatrix} \hat{\eta}_1 \\ \hat{\eta}_2 \\ \vdots \\ \hat{\eta}_{n-r} \end{pmatrix} = \begin{pmatrix} \hat{\phi}_{r+1}(x) \\ \hat{\phi}_{r+2}(x) \\ \vdots \\ \hat{\phi}_n(x) \end{pmatrix} \quad (17)$$

Finally, the asymptotic estimate for the mapping (8) is identified as

$$\Phi(\hat{x}) = \text{col}\{\hat{\phi}_1^1(\hat{x}), \dots, \hat{\phi}_{r_1}^1(\hat{x}), \dots, \hat{\phi}_1^m(\hat{x}), \dots, \hat{\phi}_{r_m}^m(\hat{x}), \hat{\phi}_{r+1}(\hat{x}), \dots, \hat{\phi}_n(\hat{x})\} \in \mathfrak{R}^n \quad (18)$$

Theorem 2

Suppose that system (1)–(3) is locally detectable in the sense of Definition 1 and the measured outputs are corrupted with noise which is a Lebesgue-measurable function of time with maximal magnitude ε . Then the higher-order sliding-mode observer (13), (14), (19), (21) ensures a state observation error accuracy of the order of $\varepsilon^{2/(\bar{r}+1)}$, $\bar{r} = \max r_i, i = 1, \dots, m$.

Theorem 3

Suppose that the outputs of system (1)–(3) are measured at discrete sampling times with a sufficiently small sampling interval δ . Then the higher-order sliding-mode observer (13), (14), (19), (21), after some transient, ensures a state observation error accuracy of the order of δ^2 .

Remark

When the total the relative degree of the system $r = n$, all the states

By direct computation, it follows that

$$L_g h(x) = 0, \quad L_g L_f h(x) = 1$$

and thus the system (22)–(23) has global relative degree 2. Choose the coordinate transformation as $T : \xi_1 = x_1, \xi_2 = x_2, \eta = x_1^2 x_3$. Note that for $x_1 \neq 0$, this transformation is invertible and an analytic expression for the inverse can be obtained as $x_1 = \xi_1, x_2 = \xi_2, x_3 = \eta/\xi_1^2$, since $x_1 = \rho$ is the distance of the satellite from the centre of the Earth $x_1 \neq 0$. It follows that in the new coordinate system $\text{col}(\xi_1, \xi_2, \eta)$, system (22)–(23) can be described by

$$\dot{\xi}_1 = \xi_2$$

$$\dot{\xi}_2 = \frac{\eta^2}{\xi_1^3} - \frac{k_1}{\xi_1^2} + d$$

$$\dot{\eta} = -k_2 \eta$$

Clearly, the system internal dynamics are asymptotically stable since $k_2 > 0$. Therefore, system (21)–(22) is locally asymptotically observable. From (13) and (14), the higher-order sliding-mode differentiator is described by

$$z_0^1 = v_0^1$$

$$v_0^1 = -\lambda_0^1 |z_0^1 - y|^{2/3} \text{sign}(z_0^1 - y) + z_1^1$$

$$z_1^1 = v_1^1$$

$$v_1^1 = -\lambda_1^1 |z_1^1 - v_0^1|^{1/2} \text{sign}(z_1^1 - v_0^1) + z_2^1$$

$$z_2^1 = -\lambda_2^1 \text{sign}(z_2^1 - v_1^1)$$

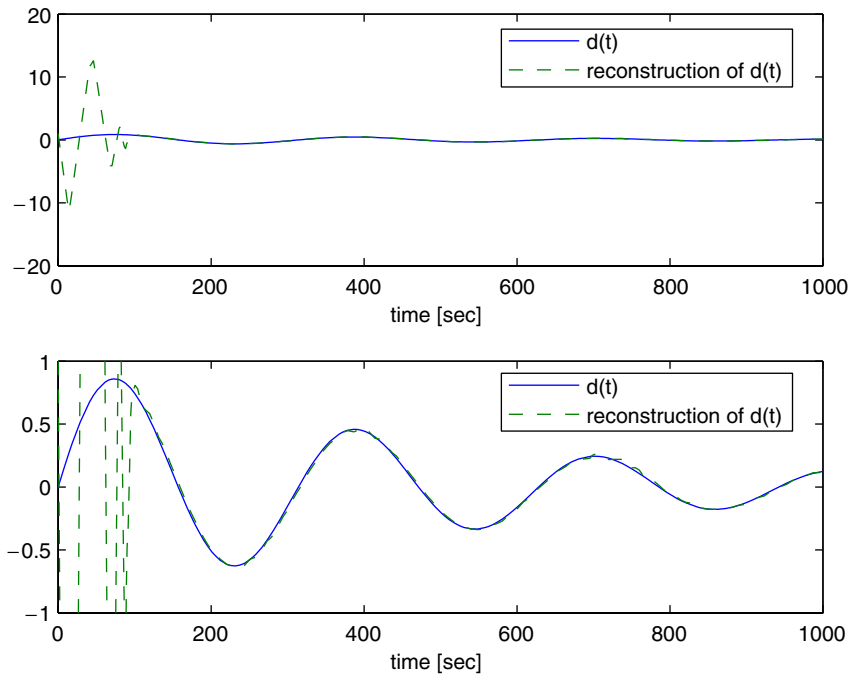
Define $\hat{\xi}_1 = z_0^1, \hat{\xi}_2 = z_1^1, \hat{\xi}_2 = z_2^1$. Then,

$$\hat{\xi} := \begin{bmatrix} \hat{\xi}_1 \\ \hat{\xi}_2 \end{bmatrix} \in \mathfrak{R}^2$$

is an estimate of ξ and the estimate for η can be obtained from the equation $\dot{\hat{\eta}} = -k_2 \hat{\eta}$. Therefore, the estimate of the disturbance $d(t)$ is available online, and from (21),

$$\hat{d}(t) = \hat{\xi}_2 - \frac{\hat{\eta}^2}{\hat{\xi}_1^3} + \frac{k_1}{\hat{\xi}_1^2}$$

is a reconstruction for the disturbance $d(t)$. As in [17], the parameters have been chosen as follows: $m = 10, M = 5.98 \times 10^{24}, k_g = 6.67 \times 10^{-11}$ and $\theta = 2.5 \times 10^{-5}$. For simulation purposes, choose $d(t) = e^{-0.002t} \sin(0.02t)$. The differentiator gains λ_i^j are chosen as $\lambda_0^1 = 2$ and $\lambda_1^1 = \lambda_2^1 = 1$. In the following simulation, the initial values $x_0 = (10^7, 0, 6.3156 \times 10^{-4})$ for the plant states in the original coordinates whilst for the observer $z_0 = (1.001 \times 10^7, 0, 1)$ and $\hat{\eta}_0 = 6.3156 \times 10^{-4}$ (in the transformed coordinate system). Figures 1 and 2 show that the states and the disturbance signal $d(t)$ can be reconstructed faithfully.

Figure 1. The disturbance signal $d(t)$ and its reconstruction signal $\hat{d}(t)$.*Example 2*

Consider the fifth-order nonlinear system

$$\dot{x} = \underbrace{\begin{bmatrix} -2x_1 - x_2 \\ x_1 \\ -x_3^3 - 2x_3 - x_4 \\ x_3 \\ (x_2 - 4)\frac{2x_5 + \sin x_5}{2 + \cos x_5} \end{bmatrix}}_{f(x)} + \underbrace{\begin{bmatrix} 1 & 0 \\ 0 & 0 \\ 0 & 1 + (2x_5 + \sin(x_5))^2 \\ 0 & 0 \\ 0 & 0 \end{bmatrix}}_{G(x)=[g_1(x), g_2(x)]} \underbrace{\begin{bmatrix} \varphi_1(t) \\ \varphi_2(t) \end{bmatrix}}_{\varphi(t)} \quad (24)$$

$$\begin{aligned} y_1 &= h_1(x) = x_2 \\ y_2 &= h_2(x) = x_4 \end{aligned} \quad (25)$$

in the domain $\Omega = \{(x_1, x_2, x_3, x_4, x_5) \mid |x_2| < 3.5, x_1, x_3, x_4, x_5 \in \mathfrak{R}\}$, where $x \in \mathfrak{R}^5$ is the system state, $y = \text{col}(y_1, y_2)$ is the system output, and $\varphi(t) = [\varphi_1(t) \varphi_2(t)]^T$ is the system input which will be reconstructed.

By direct computation, it follows that

$$L_{g_1} h_1 = L_{g_2} h_2 = 0$$

HIGHER-ORDER SLIDING-MODE OBSERVER

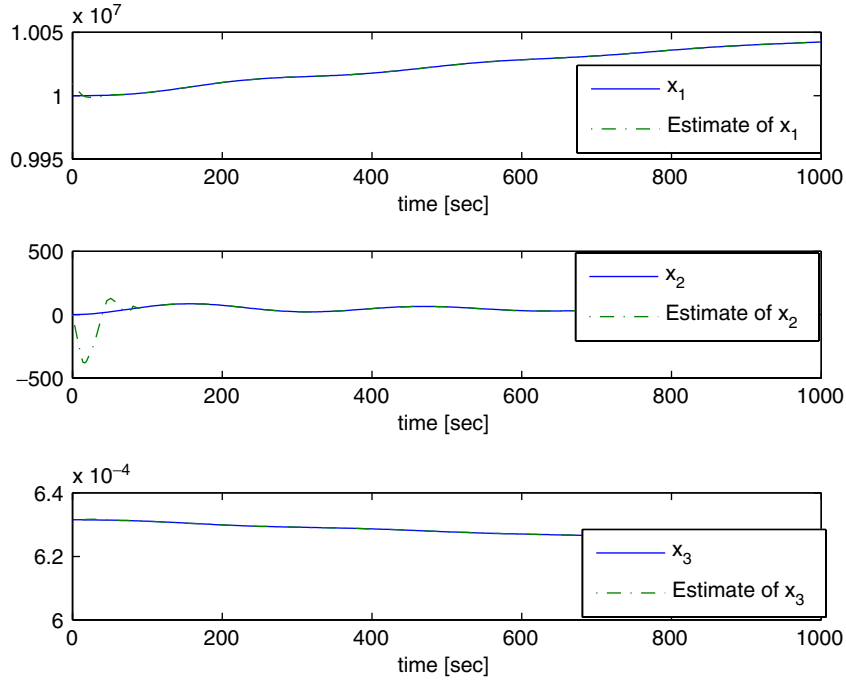


Figure 2. The response of system states and their estimates.

and

$$\begin{bmatrix} L_{g_1} L_f h_1 & L_{g_2} L_f h_1 \\ L_{g_1} L_f h_2 & L_{g_2} L_f h_2 \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ 0 & 1 + (2x_5 + \sin x_5)^2 \end{bmatrix}$$

which is nonsingular in $\mathfrak{R}^5$. Therefore, system (24)–(25) has relative degree $\{2, 2\}$. Further, $\Phi = \text{span}\{g_1, g_2\}$ is an involutive distribution and thus Assumptions (i)–(iii) are satisfied. This implies that system (24)–(25) is weakly observable in the domain Ω . Then, under the coordinate transformation: $\xi_1^1 = x_2$, $\xi_2^1 = x_1$, $\xi_1^2 = x_4$, $\xi_2^2 = x_3$, $\eta = 2x_5 + \sin x_5$, the system (22)–(23) in the new coordinate system can be described by

$$\dot{\xi}_1^1 = \xi_2^1$$

$$\dot{\xi}_2^1 = -2\xi_2^1 - \xi_1^1 + \varphi_1(t)$$

$$\dot{\xi}_1^2 = \xi_2^2$$

$$\dot{\xi}_2^2 = -(\xi_2^2)^3 - \xi_1^2 - 2\xi_2^2 + (1 + \eta^2)\varphi_2(t)$$

$$\dot{\eta} = (\xi_1^1 - 4)\eta$$

It is clear that it is not possible to obtain an analytic inverse for the inverse transformation because the fifth coordinate x_5 cannot be expressed analytically as a function of η since $\eta = 2x_5 + \sin x_5$.

Clearly, the system internal dynamics are asymptotically stable in the domain Ω . Therefore, system (24)–(25) is locally asymptotically observable. From (13) and (14), the high-order sliding-mode differentiator (13) is described by

$$\begin{aligned} \dot{z}_0^1 &= v_0^1 \\ v_0^1 &= -\lambda_0^1 |z_0^1 - y_1|^{2/3} \operatorname{sign}(z_0^1 - y_1) + z_1^1 \\ \dot{z}_1^1 &= v_1^1 \\ v_1^1 &= -\lambda_1^1 |z_1^1 - v_0^1|^{1/2} \operatorname{sign}(z_1^1 - v_0^1) + z_2^1 \\ \dot{z}_2^1 &= -\lambda_2^1 \operatorname{sign}(z_2^1 - v_1^1) \\ \dot{z}_0^2 &= v_0^2 \\ v_0^2 &= -\lambda_0^2 |z_0^2 - y_2|^{2/3} \operatorname{sign}(z_0^2 - y_2) + z_1^2 \\ \dot{z}_1^2 &= v_1^2 \\ v_1^2 &= -\lambda_1^2 |z_1^2 - v_0^2|^{1/2} \operatorname{sign}(z_1^2 - v_0^2) + z_2^2 \\ \dot{z}_2^2 &= -\lambda_2^2 \operatorname{sign}(z_2^2 - v_1^2) \end{aligned}$$

Define $\hat{\xi}_1^1 = z_0^1$, $\hat{\xi}_2^1 = z_1^1$, $\hat{\xi}_2^1 = z_2^1$, $\hat{\xi}_1^2 = z_0^2$, $\hat{\xi}_2^2 = z_1^2$, $\hat{\xi}_2^2 = z_2^2$. Then,

$$\hat{\xi} := \begin{bmatrix} \hat{\xi}_1 \\ \hat{\xi}_2 \end{bmatrix} := \begin{bmatrix} \hat{\xi}_1^1 \\ \hat{\xi}_2^1 \\ \hat{\xi}_1^2 \\ \hat{\xi}_2^2 \end{bmatrix} \in \mathfrak{R}^4$$

is an estimate of ξ and the estimate for η can be obtained from equation

$$\dot{\hat{\eta}} = (\hat{\xi}_1^1 - 4)\hat{\eta}$$

Therefore,

$$\hat{\varphi}(t) = \begin{bmatrix} \dot{\hat{\xi}}_2^1 + \hat{\xi}_1^1 + 2\hat{\xi}_2^1 \\ (\dot{\hat{\xi}}_2^2 + (\hat{\xi}_2^2)^2 + \hat{\xi}_1^2 + 2\hat{\xi}_2^2)/(1 + \hat{\eta}^2) \end{bmatrix}$$

is available online and from (19) it is a reconstruction for the input $\varphi(t)$. For simulation purposes, choose $\varphi_1(t) = \sin(0.5t)$ and $\varphi_2(t) = 0.5 \sin(0.5t) + 0.5 \cos t$. From [16], λ_i^j can be chosen as $\lambda_0^1 = \lambda_0^2 = 3$, $\lambda_1^1 = \lambda_1^2 = 1.5$, and $\lambda_2^1 = \lambda_2^2 = 1.1$. The simulation with the initial values $x_0 = (0, 0.1, 0, -0.2, 0.2)$, $z_0 = (0, 0, 0, -0.2, 0)$, and $\hat{\eta}_0 = 0.5$ are shown in the following figures. Figure 3 shows the states and the estimates in the original coordinate system. Here only asymptotic convergence is achieved. To obtain the values of $\hat{x}$ in terms of $\hat{\xi}$ and $\hat{\eta}$, it has been necessary to embed in the simulation an iteration scheme to extract $\hat{x}_5$ from

HIGHER-ORDER SLIDING-MODE OBSERVER

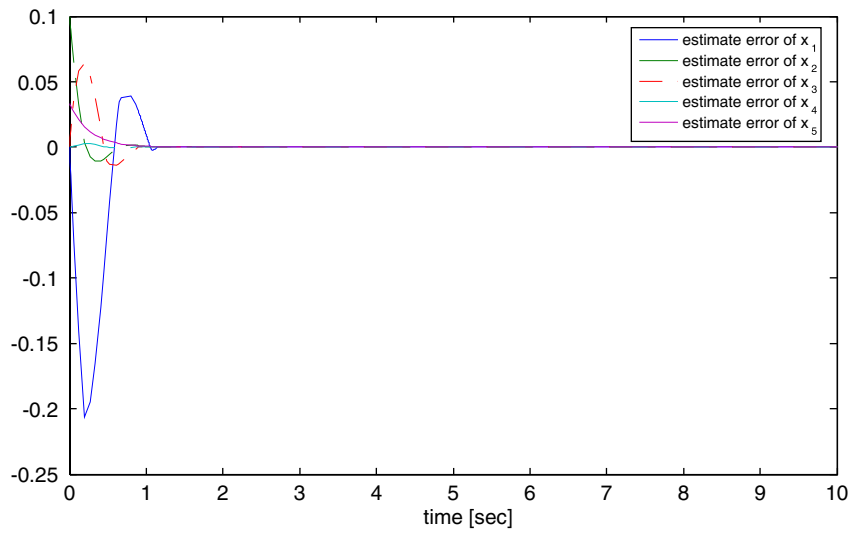


Figure 3. The original state variables $x(t)$ and their estimates $\hat{x}(t)$.

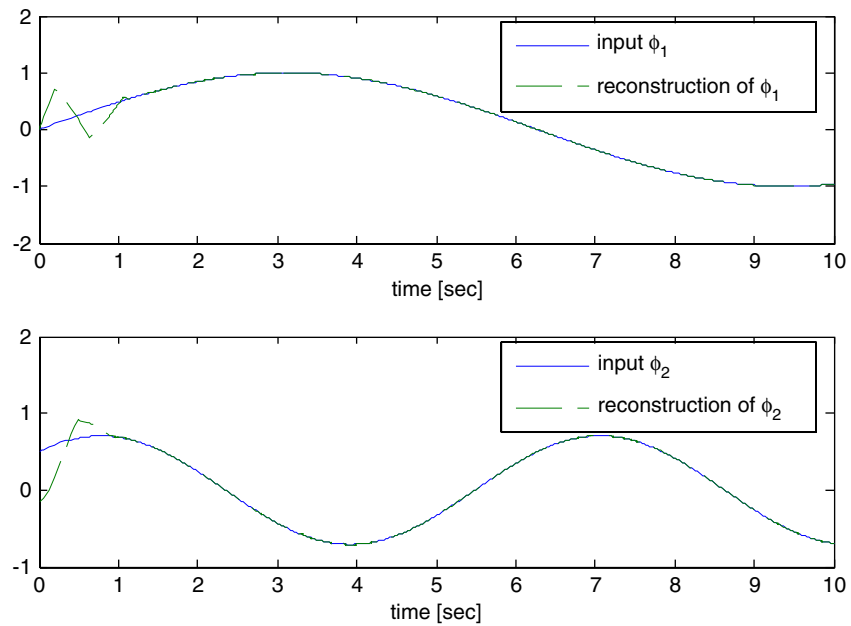


Figure 4. The inputs of system (22)–(23) and their reconstruction signal.

$\hat{\eta} = 2\hat{x}_5 + \sin \hat{x}_5$ given $\hat{\eta}$. Figure 4 shows the estimate of the unknown inputs. From the simulation, it is observed that the proposed strategy can reconstruct the input faithfully after approximately 1.1 s.

5. CONCLUSIONS

In this paper, an exact observer scheme for nonlinear locally detectable systems with unknown inputs has been proposed based on higher-order sliding-mode concepts. The approach is applicable for a class of nonlinear systems with unknown inputs, which enter affinely. The systematic design approach consists of two steps: first the transformation of the system to the Brunovsky canonical form; and second the application of higher-order sliding-mode differentiators for each coordinate of the output vector error.

The proposed scheme ensures exact finite state estimation for the observable variables and asymptotic exact estimation of the unobservable variables for the case when the system has stable internal dynamics. When the total the relative degree of the system $r = n$, all the states are estimated in finite time. In addition to estimating the states, the unknown inputs can also be identified asymptotically.

REFERENCES

1. Nijmeijer H, Fossen TI (eds). *New Directions in Nonlinear Observer Design*. Springer: Berlin, 1999.
2. Utkin V, Guldner J, Shi J. *Sliding Modes in Electromechanical Systems*. Taylor & Francis: London, 1999; 105–115.
3. Edwards C, Spurgeon SK. *Sliding Mode Control*. Taylor & Francis: London, 1998.
4. Boukhabza T, Djemai M, Barbot JP. Implicit triangular observer form dedicated to a sliding mode observer for systems with unknown inputs. *Asian Journal of Control* 2003; **5**(4):513–528.
5. Davila J, Fridman L, Levant A. Second-order sliding-mode observer for mechanical systems. *IEEE Transactions on Automatic Control* 2005; **50**(11):1785–1789.
6. Edwards C, Spurgeon SK, Tan CP. On development and applications of sliding mode observers. In *Variable Structure Systems: Towards XXIst Century*, Xu J, Xu Y (eds), Lecture Notes in Control and Information Science. Springer: Berlin, Germany, 2002; 253–282.
7. Xu J-X, Hashimoto H. Parameter identification methodologies based on variable structure control. *International Journal of Control* 1993; **57**(5):1202–1220.
8. Ahmed-Ali T, Lamnabhi-Lagarigue F. Sliding observer-controller design for uncertain triangular nonlinear systems. *IEEE Transactions on Automatic Control* 1999; **44**(6):1244–1249.
9. Floquet T, Barbot J. A canonical form for the design of unknown input sliding mode observers. In *Advances in Variable Structure and Sliding Mode Control*, Edwards C, Fossas E, Fridman L (eds), Lecture Notes in Control and Information Science. Springer: Berlin, 2006; 271–292.
10. Bejarano FJ, Poznyak A, Fridman L. Observer for linear time invariant systems with unknown inputs based on the hierarchical super-twisting concept. *Proceedings of the 9th Workshop on Variable Structure Systems*, Algero, Italy, 2006; 208–213.
11. Fridman L, Levant A, Davila J. High-order sliding-mode observation and identification for linear systems with unknown inputs. *Proceedings of the 45th Conference on Decision in Control*, San Diego, CA, 13–15 December 2006; 5567–5572.
12. Bejarano FJ, Poznyak A, Fridman L. Robust exact state reconstruction via hierarchical second order sliding mode. *Proceedings of the Annual Congress of the Mexicana de Control Automatico*, Cuernavaca, Mexico, 2005.
13. Levant A. Robust exact differentiation via sliding mode technique. *Automatica* 1998; **34**(3):379–384.
14. Levant A. High-order sliding modes: differentiation and output-feedback control. *International Journal of Control* 2003; **76**(9–10):924–941.
15. Isidori A. *Nonlinear Control Systems* (3rd edn). Springer: Berlin, 1995; 219–290.
16. Krener AJ, Respondek W. Nonlinear observers with linearizable error dynamics. *SIAM Journal of Control and Optimization* 1985; **23**(2):197–216.
17. Zhang Q. A new residual generation and evaluation method for detection and isolation of faults in nonlinear systems. *International Journal of Adaptive Control and Signal Processing* 2000; **14**(7):759–773.